

Irradiation induced defects by Fe-ion in 316L stainless steel studied by Positron Annihilation Spectroscopy

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Keywords: 316L; Fe-ion irradiation; Positron annihilation; Vacancy; Irradiation defects

Abstract. Solution annealed type 316L austenitic stainless steels were irradiated using 2 MeV Fe ions at room temperature. The implanted fluences were 2×10^{12} ions/cm² and 1×10^{13} ions/cm², respectively. Variable mono-energetic positron beam was performed to characterize the evolution of microstructure and irradiation induced defects. Results show that large amount of vacancy defects formed after heavy ion irradiation. In which, some of mono-vacancies might migrate to form small-sized clusters at room temperature. After irradiation, implanted Fe atoms mainly be interstitials atoms, but some Fe atoms might recombine with vacancies due to their high mobility, which could decrease the defect concentration, effectively.

Introduction

FeCrNi austenitic stainless steels are important structural materials for nuclear system [1-3]. Irradiation damage by energetic particles lead to the change of material properties, such as embrittlement, hardening and void swelling [1, 4-5]. The degradation of solid properties was related to the microstructural evolution [2]. Microdefects, such as dislocations, interstitials, vacancies and small-sized clusters, would formed after irradiation. Some of these microdefects might aggregate to form larger clusters, microvoids and dislocation loops. Previous studies showed that irradiation condition such as irradiation dose, temperature and the alloy elements may affect the microstructural evolution [6-8]. The size of vacancy clusters increases with increasing irradiation dose, and the cluster size would reaches 0.55 nm in diameter at 100 dpa in heavy-ion irradiated 316 stainless steel [6]. A transient stage usually existed before steady void swelling occurs with low damage dose. Theoretical and experimental analyses have revealed the importance of an incubation dose before steady state of the void swelling [9-10]. However, most of the experimental studies focused on the void formation and dislocation loops by transmutation electron microscopy (TEM). Few works focused on the point defects and small-sized clusters at low irradiation dose for the limitation of effective analysis methods. Due to its self-seeking and non-destructive nature, positron annihilation techniques are suitable to characterize the small-sized defects, such as monovacancies, and tiny vacancy clusters, dislocations, precipitates and their evolution characteristic [11-12]. Especially, variable mono-energetic positron beam is very effective to characterize the depth distribution with implanted ions trajectory.

Charged self-ion irradiation was usually used to emulate displacement damage induced by neutrons in the structural materials, which could eliminate the effect of impurity. Additionally, it could reduce the irradiation time and avoid the activation of the irradiated material. In the present study, 2 MeV Fe-ion irradiation was performed to the type 316L stainless steels with different fluences at room temperature. Positron annihilation spectroscopy was adopted to characterize the structures of irradiation induced defects.

Experimental detail

Table 1. Chemical compositions of 316L stainless steel in wt%.

Material	Fe	Cr	Ni	Mn	Mo	Cu	C	Si	P	S	N	Co
316L	Bal.	17.35	11.13	1.16	2.12	0.314	0.023	0.659	0.03	0.002	0.046	0.104

In this research, the composition of commercial 316L stainless steel is shown in Table 1. The size of the samples is $10 \times 10 \times 1 \text{ mm}^3$. All samples were mechanically polished with sandpapers and $1.5 \text{ }\mu\text{m}$ diamond spray to a mirror like surface, and then all samples were annealed at 1323 K in vacuum ($<10^{-4} \text{ Pa}$).

Fe-ion irradiation experiments were performed on the 320 kV multi-discipline research platform at the Institute of Modern Physics, CAS. The irradiation fluences was about $2 \times 10^{12} \text{ ions/cm}^2$ and $1 \times 10^{13} \text{ ions/cm}^2$, respectively. The distribution of displacement damage induced by ion irradiation and the deposition of implanted Fe ions were calculated by SRIM code [13]. The results are shown in Fig. 1. The displacement energy (E_d) of Fe atom is 40 eV in the calculation [14].

Positron annihilation spectroscopy measurements were performed using a variable mono-energetic positron facility. Positrons were generated by a ^{22}Na radiation source, and then moderated by tungsten mesh. Beam energy varied from 0.68 to 20.18 keV during Doppler broadening energy spectroscopy measurement. The microstructural evolution in the specimens could be characterized though the conventional S and W parameters. The S parameter is defined as the ratio of counts in the central energy region around 511 keV (510.24 – 511.76 keV) to the total counts at the energy region between 504.2 keV and 517.8 keV, which means positron annihilated with valence electron and sensitive to the defect concentration. The W parameter is the ratio of the counts in the wing area (504.2 - 508.4 keV and 513.6 – 517.8 keV) to the total counts around 504.2 – 517.8 keV, which represent the positron annihilated with core electron and related to the chemical composition.

The mean implantation depth of the energetic positrons is estimated by the incident energy and calculated by the following equation [15]:

$$Z(E) = \left(\frac{40}{\rho}\right) E^{1.6} \quad (1)$$

where $Z(E)$ is expressed in units of nanometer, ρ is the material density of 316L stainless steel. E is the incident positron energy in keV.

Positron annihilation lifetime spectroscopy measurements were also performed by variable-energy slow positron beam [16]. The continuous positron beam was transformed into a pulsed system by the pulsing system, which consists of a reflection type chopper, a prebuncher and a buncher [17]. A BaF_2 scintillation detector was employed to obtain the signal of positron annihilation. The stop signal for the positron lifetime measurement come from the pulsing electronic system, and the start signal is derived from the detector. The time resolution of this system is about 386 ps. In measurement, positrons energy were selected to 2 keV and 12 keV, which related to the implanted depth were 16 nm and 285 nm, respectively. Over 1.3×10^6 counts were collected for each spectrum.

Results and discussion

Fig. 1 shows the results of SRIM calculation. From Fig. 1, certain amount of vacancy-type defects would be generated after Fe-ion irradiation. Irradiation induced vacancies distributed from surface to about $1 \text{ }\mu\text{m}$, and peaked at about 600 nm. The implanted Fe atoms mainly deposited between 300 nm and $1 \text{ }\mu\text{m}$, and the depth of deposition peak was about 750 nm. The damage dose at peak was about $4.6 \times 10^{-3} \text{ dpa}$ and $2.3 \times 10^{-2} \text{ dpa}$, respectively.

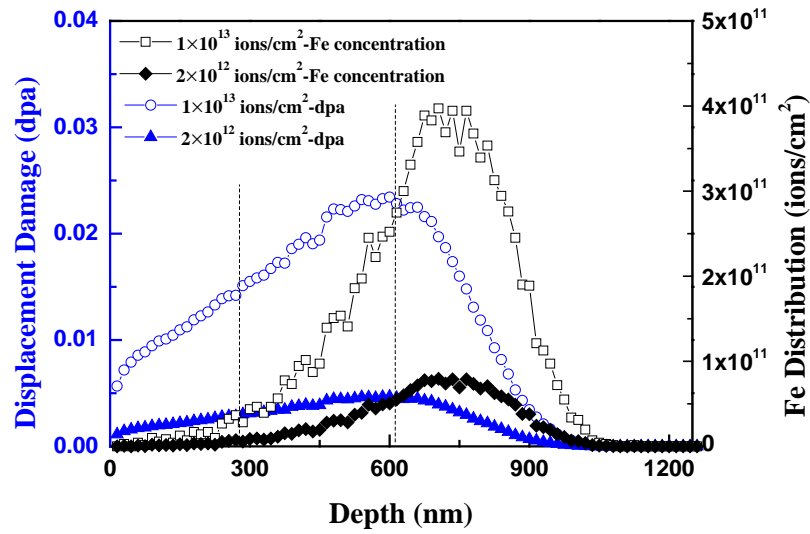


Figure 1. Depth profiles of the displacement damage and implanted Fe ions calculated by SRIM.

Fig. 2 shows the variation of S parameters as a function of incident positron energy. The average incident depth of energetic positrons is shown on the top x-axis. For the unirradiated specimen, the value of S parameter is largest at surface layer, and then decreased rapidly. This phenomenon could be explained by the affection of surface defects or the effect of positron diffusing back to the surface and the formation of ortho-positronium [18]. At last, the saturated S value of the unirradiated specimen is around 0.38. Compared to the unirradiated specimen, similar variation trend of S parameter would be observed at surface layer for two irradiated specimens. However, the S value kept almost constant with the depth over 48 nm for both irradiated specimens, and it would be larger at higher irradiation dose. These results indicate that certain amount of vacancy-type defects formed after Fe-ion irradiation even though at low damage dose.

In order to characterize the surface effect, variable mono-energetic positron annihilation lifetime measurement was performed on the post-irradiated specimens with the positron energy of 2 and 12 keV. The mean implanted depth of positrons are about 16 and 285 nm, respectively. The normalized positron annihilation lifetime spectra **are shown** in Fig. 3. Similar spectra is observed for two samples with different damage dose at the same depth. However, the counts intensity of the surface layer are larger than the inner layers at long lifetime region, obviously. One reason is that some of the incident positrons with low energy might backscattered from the surface, and then implanted into the solid again, which prolonged their annihilation lifetime. As reported, some of the incident positrons would form ortho-positronium at the surface of metals [19]. The lifetime of o-Ps could be several nanoseconds, which explained the long lifetime part of the surface layer as shown in Fig. 3.

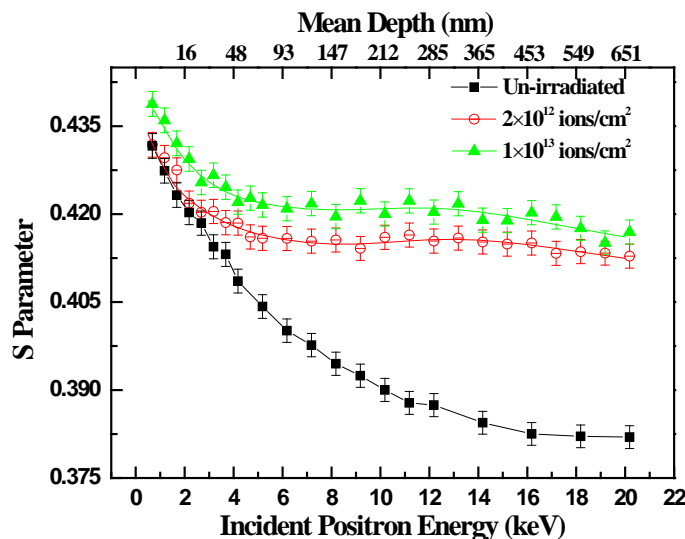


Figure 2. S parameters as a function of incident positron energy for the samples with different irradiation fluences.

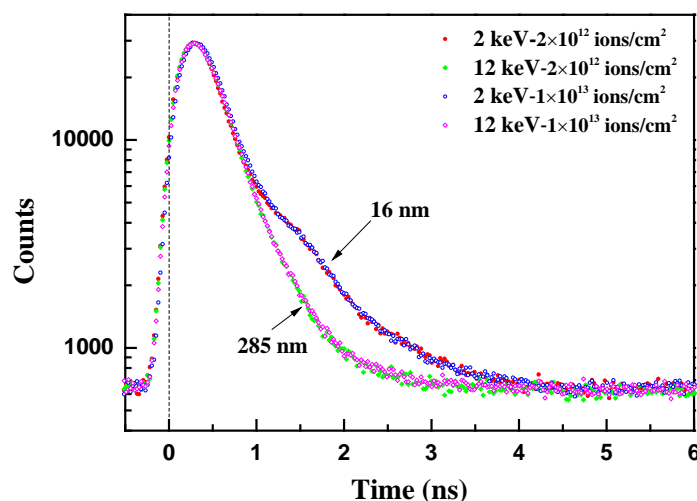


Figure 3. Positron annihilation lifetime spectra of the post-irradiated specimens at surface and damage region, respectively.

S-E curves were analyzed by the VEPFIT, which is based on the multi-layer structures of positron diffusion model [20]. The VEPFIT analysis of the experimental data was divided into four layers. The first layer is the surface layer. According to the SRIM calculation, as shown in Fig. 1, the damage region is divided into three layers. The second layer is the track region, where the implanted Fe ions slow down through atomic collision. However, Fe atom was hardly deposited in this layer. At the same time, certain amount of vacancy defects were generated in this layer. The third layer is the damage region. Much more vacancy defects induced by Fe-ion irradiation were generated here, and part of the implanted Fe atoms would stay in this layer. The fourth region is called deposited region, where most of the implanted Fe atoms stay in this layer, and part of the damage defects were also generated here. Fig. 4 shows the fitted S parameters as a function of depth for the irradiated specimens. The boundaries of these four layers are about 0-20, 20-300, 300-600 and 600-651 nm, respectively. Similar variation trend of the fitted S parameter can be observed for both irradiated specimens, and the fitted value for higher dose specimen are always larger than the lower dose specimen. Neglecting the surface layer, the fitted S value should be largest at damage layer, and then is the track region. It would be smallest at the deposited region. For the reason that the value of S parameter is related to the effective defect concentration. The defect density at damage layer (300-600 nm) would be larger than the other two layers.

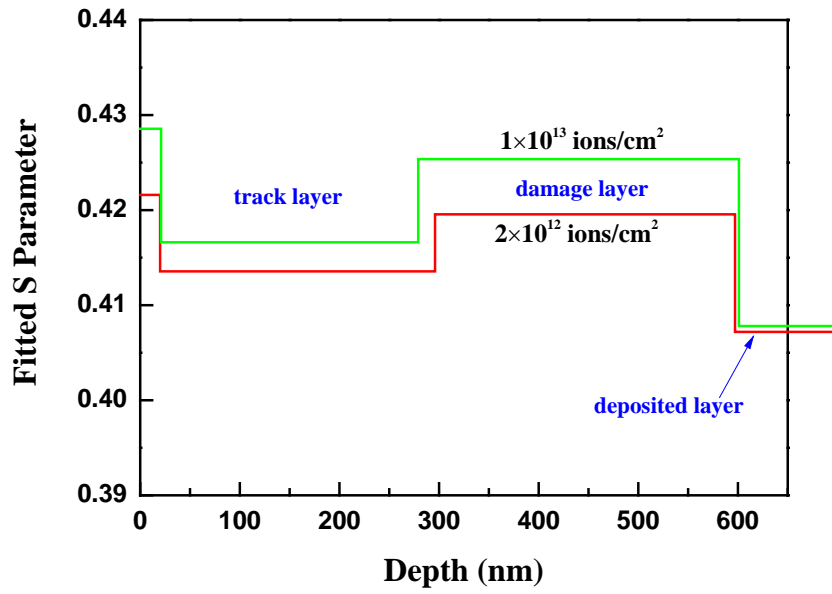


Figure 4. Fitted S parameters of the post-irradiated specimens at different depth region using VEPFIT

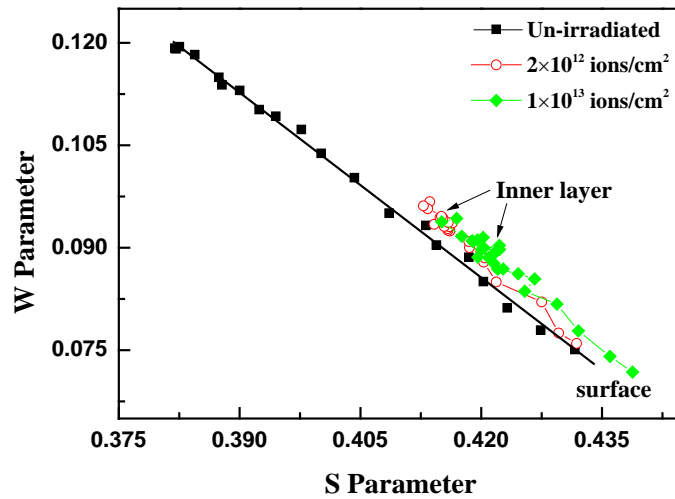


Figure 5. S-W plots for the irradiated specimens with different fluences.

Information about the type of defects in specimens could be revealed by plotting the W parameter as a function of the S parameter. The S-W plots for the unirradiated and post-irradiated alloys are shown in Fig. 5. For the defect free specimen, the S-W plot can be fitted to a linear function because of the similar positron annihilation mechanism at the annihilation site. Compared to the unirradiated sample, the (S, W) points of the post-irradiated samples were aggregate and deviate from the defect free sample. This might indicate that the microstructure was changed and only one type of micro defects generated after self-ion irradiation.

Fe atoms is one of the main elements in 316L stainless steel so that no other impurities would be induced after Fe-ion irradiation. Therefore, displacement damage is the only reason for the variation of the S parameter in the irradiated specimens. Large amount of vacancies would be formed after energetic Fe ions implanted into the alloy by SRIM calculation. The damage dose also increased at higher fluence, which could induce much more vacancies in the solid. In addition, mono-vacancies was not stable even at room temperature because of their low migration energy [14]. They could migrate and aggregate to form vacancy clusters even at room temperature in steel [21]. However, the vacancy clusters could not migrate with the temperature lower than $0.3T_m$ (T_m is the melting

temperature of steel) [14]. They **could** exist in the solid stably. Meanwhile, several impurity atoms **could** trap the mobile mono-vacancies to form impurity-vacancy complexes [15, 22]. These complexes **were** hardly migrate at room temperature due to their larger migration energy compare to the mono-vacancies. These impurity-vacancy complexes can be divided into interstitial or substitutional type. As the Fe ions implanted into the solid, most of them would form self-interstitial atoms (SIAs), firstly. Some of them might recombine with the irradiation induced vacancies. Due to the low damage dose in this experiment and the limitation of the irradiation temperature, no void formed in the solid. The microdefects **would be** mono-vacancies, small clusters, impurity-vacancy complexes and interstitials, according to the above analysis. The migration energy of interstitials is usually lower than vacancies so that they **could** move easily and recombine with vacancy defects, which **could** reduce the effective concentration of vacancy defects. The variation of S parameter is related to the size or the concentration of vacancy-type defects. As the fitted S parameter shown in Fig. 4, the value of S parameter in track layer would be lower than that in damage layer. This indicates that less vacancy defects was performed in the track region, and most of the monovacancies and clusters **would be** generated at damage layer. Even though small part of Fe atoms **would** deposited at this region to form self-interstitial atoms and some of them **would** recombine with mono-vacancies. Most of the incident atoms **would** deposited at the depth over 600 nm which meant large amount of interstitials formed at this region. While the defects concentration decreased sharply according to the SRIM calculation. These interstitials **was** unstable for the reason of their high mobility, which **could** decrease the defect concentration, obviously.

Conclusion

Fe ion irradiation was conducted to the type 316L stainless steel with different damage dose at room temperature. The evolution of microstructure was investigated by variable mono-energetic positron annihilation techniques. Some of the incident positrons with low energy might backscattered from the surface, which prolong the annihilation lifetime. Large amount of vacancy-type defects generated after heavy ion irradiation even though the damage dose **was** low. The defect concentration also **varied** at different depth layer. Implanted Fe atoms **would** be interstitials, and some of them **would** recombine with vacancies due to the high mobility. This effect **would** decrease the effective concentration of the vacancy-type defects.

Acknowledgement

This work is supported by the National Science Foundation of China 91226103, 11475193 and 11475197. The authors greatly appreciate all the help from the staff of 320 kV multi-discipline research platform at the Institute of Modern Physics, CAS during the heavy ion irradiation.

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